

# Scaling of early afterslip velocity and possible detection of tsunami-induced subsidence by GPS measurements immediately after the 2011 Tohoku-Oki earthquake

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## SUMMARY

We explore the use of on-land GPS observations to detect deformation due to tsunami propagation near source regions of large interplate earthquakes. Here, we focus on the  $M_w$  9 Tohoku-oki earthquake, which occurred around 14:46 (JST) on 2011 March 11. We consider GPS data in the time span 14:54–15:22 (JST) along the Sanriku coast, where the tsunami had the largest amplitude. The displacement data shows the signatures of large aftershocks as well as post-seismic fault slip (afterslip). These effects are particularly evident in the east component. From the horizontal displacement vectors, we construct a simple fault model for the early phase of the afterslip. Mean slip velocity of the early afterslip reaches  $0.1 \text{ mm s}^{-1}$ . By compiling the early afterslip velocity of recent interplate earthquakes around that region, we find its increasing trend with the main shock magnitude. This scaling relation may reflect higher stressing rates at edges of larger main shock faults. Separately, we forward calculate land deformation due to tsunami height changes based on a tsunami simulation. Tsunami-induced deformation is only evident in the vertical direction at coastal GPS stations. The predicted subsidence amounts at some coastal stations can account for a large portion of the residuals between the observation and the modelled deformation due to the fault slip.

**Key words:** Satellite geodesy; Transient deformation; Tsunamis; Earthquake dynamics; Subduction zone processes.

## 1 INTRODUCTION

Seismic slip of the 2011 Tohoku earthquake on March 11, whose moment magnitude was  $M_w$  9, caused major deformation along the east coast of Honshu Island, Japan. A dense on-land GPS network, named GEONET, recorded the signals of the slip-induced deformation. Simons *et al.* (2011) and many other studies (e.g. Ozawa *et al.* 2011) have estimated the coseismic fault slip. Large aftershocks and afterslip were also observed by GEONET.

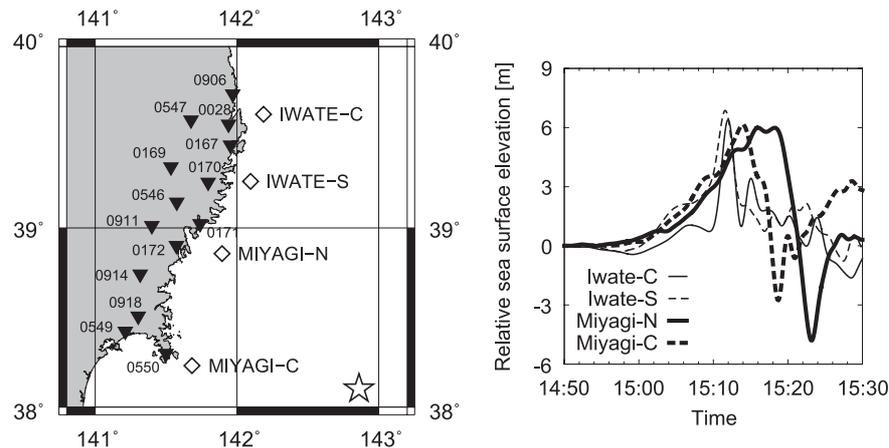
Land deformation associated with large interplate earthquakes is not limited to elastic displacement directly caused by interplate fault slip. For example, the Earth is strained temporarily by ocean mass movements (tsunamis) caused by fault slip, as revealed by teleseismic observations using strainmeters, broad-band seismometers and gravimeters for previous earthquakes (Yuan *et al.* 2005; Nawa *et al.* 2007; Takatsuka *et al.* 2008; Boudin *et al.* 2013; Jolly *et al.* 2013; Kimura *et al.* 2013). Such deformation could contaminate the signals of the slip-induced deformation near source faults, if displacements during the tsunami arrival are used.

Here, we estimate land deformation due to fault slip and tsunami near the source of the 2011 Tohoku earthquake. Regarding the former slip-induced deformation, early afterslip of the 2011 Tohoku earthquake had been reported by Munekane (2012). In this paper, we re-examine the amount of early afterslip at the time of the tsunami arrivals. Further, we focus on the latter tsunami-induced deformation because its contribution to deformation field has not yet been documented for the 2011 Tohoku earthquake. We use on-land GPS data at GEONET stations along the coast line of the Sanriku, where the tsunami after the Tohoku earthquake attacked first (Hayashi *et al.* 2011) and most heavily (Mori *et al.* 2011).

Detection of tsunami-induced land deformation by satellite observations has been tried previously (Plag *et al.* 2006) but not reported. Physically, signals of tsunami-induced deformation should stand out in vertical displacement at each GPS station, since tsunami-induced land deformation is a kind of deformation by surface loads. For instance, we can simplify the problem as elastic deformation in a half-space due to a point load, the so-called Boussinesq's problem. Lamb (1902) gave the solution for the ratio of vertical displacement  $d_v$  to tangential displacement  $d_t$  at an observation point owing to a surface point load

$$\frac{d_v}{d_t} = \frac{\lambda + 2\mu}{\mu}, \quad (1)$$

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**Figure 1.** Left-hand: map of the Sanriku coast. The solid triangles represent the GEONET stations. We call the stations numbered 0906, 0028, 0167, 0170, 0171, 0172 and 0550 as coastal stations, and 0547, 0169, 0546, 0911, 0914, 0918 and 0549 as landward stations. One more GEONET station is located between 0172 and 0550, numbered 0036, but that station did not record the deformation signal after the Tohoku earthquake. The star indicates the epicentre of the 2011 Tohoku earthquake, determined by the Japan Meteorological Agency ( $142.86^{\circ}\text{E}$ ,  $38.10^{\circ}\text{N}$ ). The open squares show the NOWPHAS stations to monitor sea surface height by GPS buoys. Right-hand panel: relative sea surface elevation after the 2011 Tohoku earthquake which occurred around 14:46.

where  $\lambda$  and  $\mu$  are the first and second Lamé constants in the elastic field. Noting that  $(\lambda + 2\mu)/\mu \simeq 3$  for crustal materials, tsunami loading on the Earth generally causes at least three times larger vertical displacement than horizontal displacement. This characteristic contrasts with slip-induced deformation by thrust faults (e.g. Okada 1992) where the ratio is typically below one.

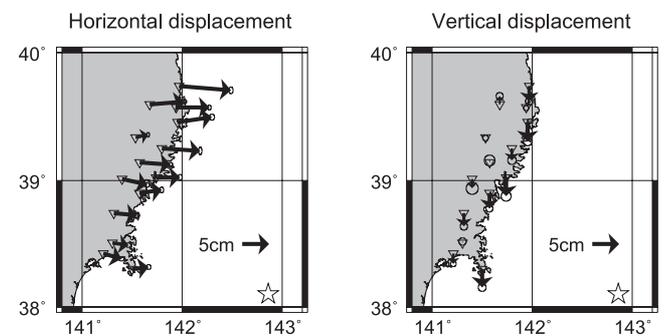
## 2 DISPLACEMENT ALONG THE SANRIKU COAST AFTER THE TOHOKU EARTHQUAKE

### 2.1 GEONET data

We use the 1 Hz-GPS data analysed using the precise point positioning method, provided by the Geospatial Information Authority of Japan (GSI) through Nippon GPS Data Services Company (NGDS) and the VERIPOS/APEX service using the RTNet software (GPS-Solutions). We focus on the GEONET stations located along the Sanriku coast (Fig. 1). For reference, the figure also indicates locations of NOWPHAS stations monitoring sea surface height by GPS buoys.

The 2011 Tohoku Earthquake occurred around 14:46 (JST) on March 11 and its seismic moment release continued over several minutes. The resulting massive tsunami propagated westward and attacked the Sanriku coast. Fig. 1 presents the records of the relative sea surface elevation after 14:50, at the NOWPHAS stations. As Maeda *et al.* (2011) and Fujii *et al.* (2011) reported, a tsunami with a smoothly increasing amplitude came first and a short-period impulsive tsunami followed.

The sea surface elevation data imply that the tsunami-induced subsidence along the Sanriku coast appeared by around 15:20. Therefore we focus on relative displacement at the GEONET stations during almost 30 min after the main shock. Since few coastal stations had recorded the time-series data after the tsunami arrivals, we do not try to detect the ‘unloading’ after the tsunami passes in this paper. Fig. 2 shows the observed horizontal and vertical displacement at the GEONET stations between the median positions at 14:54–14:56 and 15:20–15:22. All the stations moved eastward,



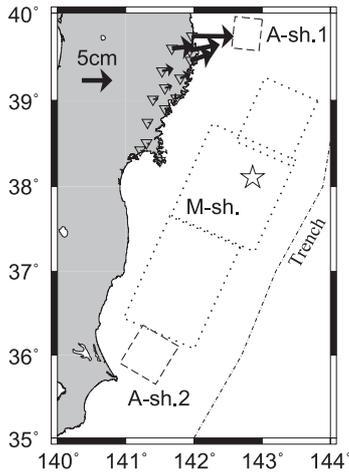
**Figure 2.** Observed horizontal (left-hand panel) and vertical (right-hand panel) displacement at the GEONET stations between the median positions at 14:54–14:56 and 15:20–15:22. For the horizontal displacement, diameters of each error ellipsoid are given by square sums of interquartile ranges for the time spans 14:54–14:56 and 15:20–15:22 in the east–west and north–south directions. For the vertical displacement, a diameter of each error circle is also given by square sums of interquartile ranges for the time spans 14:54–14:56 and 15:20–15:22 in the vertical direction.

and most of the stations subsided. We show all the time-series data in Appendix A.

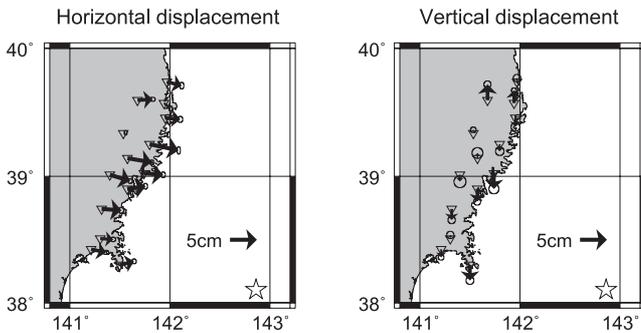
### 2.2 Deformation by large aftershocks and afterslip

The post-seismic deformation included signals of large aftershocks and afterslip on the plate interface. In particular, the horizontal displacement at the GEONET stations should be explained by the aftershocks and afterslip.

Several large (over  $M_w 7$ ) aftershocks occurred following the main shock of the 2011 Tohoku earthquake. In particular, two aftershocks, one occurred around 15:09 off Iwate ( $142.78^{\circ}\text{E}$ ,  $39.84^{\circ}\text{N}$ ), hereafter Aftershock 1, and the other occurred around 15:16 off Ibaraki ( $141.27^{\circ}\text{E}$ ,  $36.11^{\circ}\text{N}$ ), Aftershock 2, affected the displacement signals in Fig. 2. Fig. 3 shows simplified rectangular fault models of the main shock, Aftershock 1 and Aftershocks 2 estimated using on-land GPS data (Nishimura *et al.* 2011). We reconstruct the amounts of static displacement on the GEONET stations by Aftershocks 1 and 2 using a Green’s function in a homogeneous



**Figure 3.** Rectangular fault models of the main shock, Aftershock 1, and Aftershocks 2 in the previous study (Nishimura *et al.* 2011). The main shock faults are given by the three rectangles. The GEONET stations used in this study are represented by the triangles. We also plot the reconstructed horizontal displacement due to Aftershocks 1 and 2 from the previous study. The trench line is based on DeMets *et al.* (1990).

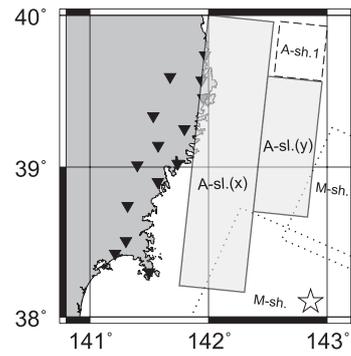


**Figure 4.** Residual displacement  $d_r$  between the observation (Fig. 2) and the aftershock-induced slip based on the previous study.

elastic half-space (Okada 1992), where the rigidity is assumed to be 40 GPa and the Poisson's ratio 0.25 (the same settings as Nishimura *et al.* 2011). Fig. 3 shows the calculated horizontal displacement due to Aftershocks 1 and 2. Although the aftershock model has uncertainties, we only plot the maximum likelihood solution.

The residual displacement vectors  $d_r$  between the observation and the aftershock-induced deformation are illustrated in Fig. 4. Since the horizontal displacement by tsunami load is negligible (we will confirm this point based on tsunami simulation models in a later section), we roughly estimate the early afterslip on the plate interface from the horizontal vectors during the observation period (from 14:54–14:56 to 15:20–15:22). Referring to the source faults of the main shock and Aftershock 1, and a geometry of the plate interface (e.g. Zhao *et al.* 2011; Hayes *et al.* 2012), we set two rectangular faults ( $x$ ) and ( $y$ ) for the afterslip as shown in Fig. 5. The afterslip faults are assumed to be separate from the source areas of the main shock and Aftershock 1. The fault parameters are given by Table 1. Slip amount of Fault ( $x$ ),  $u_x$ , and that of Fault ( $y$ ),  $u_y$ , are variables.

We estimate  $u_x$  and  $u_y$  simply by minimization of the residual sum of squares between the observation and the modelled deformation. First, we ignore the error ellipsoids of the observation.



**Figure 5.** A fault model of the afterslip given by the two rectangles ( $x$ ) and ( $y$ ) with solid lines. The afterslip faults are set to be separate from the source faults of the main shock and Aftershock 1.

Using the Green's function in a homogeneous elastic half-space (Okada 1992), we calculate displacement vectors  $d_c$  at the GEONET stations from  $u_x$  and  $u_y$ . A residual sum of squares  $S_1$  from  $d_r$  (observation minus aftershock-induced deformation) and  $d_c$  (calculated afterslip-induced deformation) for the horizontal displacement is given by

$$S_1 = \sum_{\text{stations}} [(d_r - d_c)_{\text{NS}}^2 + (d_r - d_c)_{\text{EW}}^2]. \quad (2)$$

Next, we consider the error ellipsoid of the observation at each station (Fig. 2) as weight of the residual error. We define another residual sum of squares  $S'_1$  as

$$S'_1 = \sum_{\text{stations}} \left[ \left( \frac{d_r - d_c}{D} \right)_{\text{NS}}^2 + \left( \frac{d_r - d_c}{D} \right)_{\text{EW}}^2 \right], \quad (3)$$

where  $D$  is a half width of the error ellipsoid.

Fig. 6 presents distributions of  $S_1$  and  $S'_1$  when  $u_x$  and  $u_y$  are varied. We find that  $S_1$  has a minimum value  $2.4 \times 10^{-3}$  (m<sup>2</sup>) with  $u_x = 0.18$  (m) and  $u_y = 0.19$  (m) and  $S'_1$  has a least value 220 with  $u_x = 0.13$  (m) and  $u_y = 0.24$  (m). Fig. 7 shows the calculated horizontal displacement at each station for the least  $S_1$  and  $S'_1$  models. The total moment magnitude is 7.2–7.3. Practically the differences in both models are negligible.

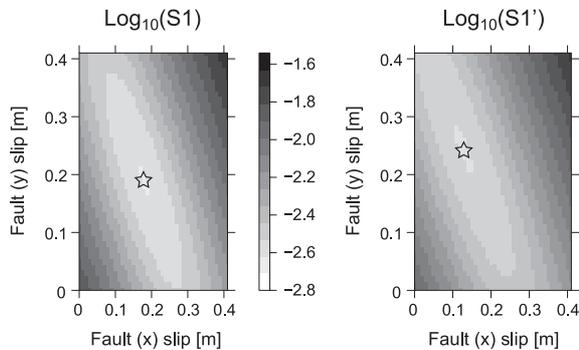
In addition, we roughly calculate the slip velocity of the afterslip based on the least  $S_1$  model. In Fault ( $y$ ), the seismic moment released from 14:54–14:56 to 15:20–15:22 was  $3 \times 10^{19}$  N m. Thus the mean rate of the moment release was as large as  $2 \times 10^{16}$  N m s<sup>-1</sup>. Under the assumption of the rigidity 40 GPa, the product of slip velocity and the slip area ( $4 \times 10^9$  m<sup>2</sup>), summed with the product of the slip amount and slip area change per unit time, was almost  $5 \times 10^5$  m<sup>3</sup> s<sup>-1</sup>. If we neglect propagation of the afterslip (the slip area change per unit time is zero), the slip velocity was on the order of  $10^{-4}$  m s<sup>-1</sup> = 0.1 mm s<sup>-1</sup>.

### 2.3 Deformation by tsunami

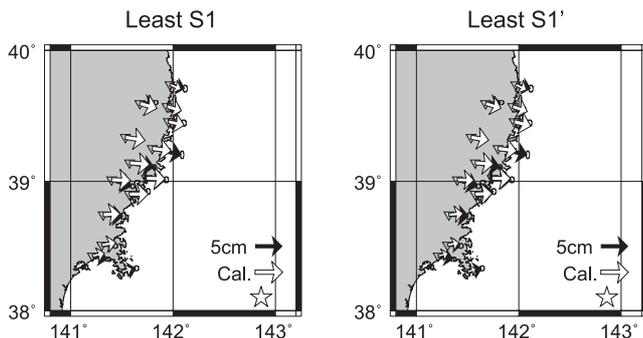
In order to evaluate the tsunami-induced displacements, we calculate the load deformation from sea height changes in a tsunami simulation (Gusman *et al.* 2012). Namely, we obtain elastostatic deformation at the on-land GPS stations by spatially convolving sea-mass loads, which are obtained from the simulated sea-height changes during 14:55–15:21, with a Green's function. The calculation method is similar to those in several studies (Farrell 1972; Matsumoto *et al.* 2001; Plag *et al.* 2006). The tsunami-induced deformation  $d_{it}$  at each observation point is given by

**Table 1.** Fault parameters for the afterslip.

Fault	Longitude <sup>a</sup> (°)	Latitude <sup>a</sup> (°)	Depth <sup>a</sup> (km)	Length (km)	Width (km)	Strike <sup>b</sup> (°)	Dip (°)	Rake <sup>c</sup> (°)
(x)	142.0	40.0	50.0	200.0	50.0	186.0	20.0	90.0
(y)	142.5	39.6	38.0	100.0	40.0	186.0	12.0	90.0

<sup>a</sup>At a northern and lower edge of rectangular fault.<sup>b</sup>Rotation angle from north (clockwise).<sup>c</sup>Rotation angle from the strike direction (counter-clockwise).

**Figure 6.** Distribution of the residual sum of squares  $S_1$  and  $S_1'$  when the slip amount of Fault (x),  $u_x$ , and the slip amount of Fault (y),  $u_y$ , are varied. (Left-hand panel:  $S_1$  has a least value  $2.4 \times 10^{-3}$  ( $m^2$ ) with  $u_x = 0.18$  (m) and  $u_y = 0.19$  (m), represented by the star. Right-hand panel:  $S_1'$  has a least value 220 with  $u_x = 0.13$  (m) and  $u_y = 0.24$  (m), also represented by the star.



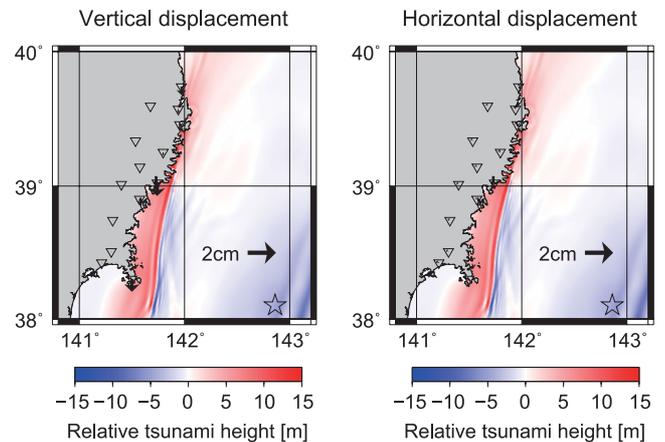
**Figure 7.** Calculated horizontal displacement for the least  $S_1$  model [ $u_x = 0.18$  (m) and  $u_y = 0.19$  (m)] and  $S_1'$  model [ $u_x = 0.13$  (m) and  $u_y = 0.24$  (m)] of the afterslip, compared with the residual displacement  $d_t$  shown in Fig. 4.

$$d_{it} = \rho A \sum_{\text{grid}} \Delta H G_f \quad (4)$$

where  $\rho$  is a water density,  $1000 \text{ kg m}^{-3}$ ,  $A$  is the grid size of the tsunami simulation,  $0.5' \times 0.5'$  (almost corresponding to  $1 \text{ km}$  square), and  $\Delta H$  is the sea-height change at each numerical grid-point. The numerical grids are located in a range of  $138^\circ\text{E}$ – $148^\circ\text{E}$  and  $34^\circ\text{N}$ – $42^\circ\text{N}$ .  $G_f$  is a Green's function for the point load

$$G_f(\theta) = \frac{r_e}{m_e} \sum_{n=0}^{\infty} h_n P_n(\cos \theta), \quad (5)$$

where  $\theta$  is an angular distance from a centre of the simulation grid to an observation point,  $r_e$  is the radius of the Earth,  $6378 \text{ km}$ ;  $m_e$  is the mass of the Earth and  $h_n$  are Love numbers depending on an assumed elastic structure of the Earth, and  $P_n$  represents



**Figure 8.** Calculated vertical and horizontal displacement from the simulated sea-height changes during 14:55–15:21, with the Green's function based on the PREM. The colour contour indicates the relative tsunami height from 15:21 to 14:55 in the tsunami simulation.

the Legendre function of degree  $n$ . Here, we use a Green's function (Pagiatakis 1990) based on PREM (Dziewonski & Anderson 1981).

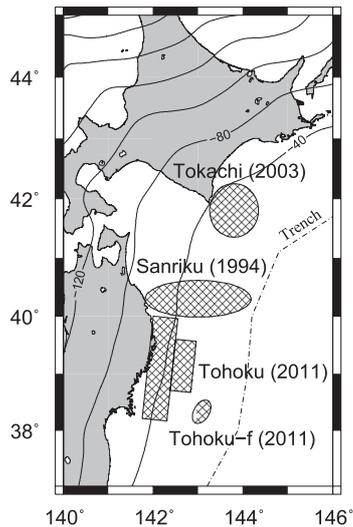
Fig. 8 shows the simulated displacement. We find that only the coastal stations subside, by  $< 1 \text{ cm}$ , although the subsidence of stations 0171 and 0550 reach nearly  $1 \text{ cm}$ . By contrast, the amounts of the vertical displacement at the landward stations are too small to be detected. As we assumed in the preceding section, the horizontal displacement by the tsunami loading are too small to be detected.

### 3 DISCUSSION

#### 3.1 Slip velocity of early afterslip at the Pacific Plate subduction zone

We estimated that the slip velocity of the early afterslip following the 2011 Tohoku earthquake off Sanriku was approximately as fast as  $0.1 \text{ mm s}^{-1}$  ( $10^{-4} \text{ m s}^{-1}$ ). Munekane (2012) also investigated the early afterslip around the same region. They estimated the slip amount was approximately  $5 \text{ cm}$  during  $10 \text{ min}$  after the main shock, which corresponds to the slip velocity of  $8 \times 10^{-5} \text{ m s}^{-1}$ . We compare these values with other cases of recent large interplate earthquakes at the Pacific Plate subduction zone.

Fig. 9 illustrates source regions of afterslip of recent large earthquakes on the Pacific subduction plate interface. Namely we focus on the 2003 Tokachi-oki earthquake ( $M_w$  8.3 by USGS and  $M_w$  8.0 by JMA), the 1994 Sanriku-oki earthquake ( $M_w$  7.7 by USGS and  $M_w$  7.6 by JMA), the 2011 Miyagi-oki earthquake of a possible

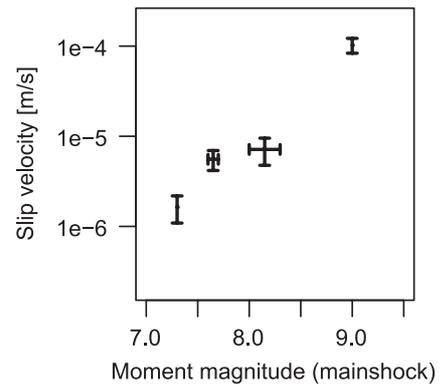


**Figure 9.** Source regions of afterslip of recent large earthquakes at the Pacific subduction plate interface: the 2003 Tokachi-oki earthquake ( $M_w$  8.3 by USGS and  $M_w$  8.0 by JMA), the 1994 Sanriku-oki earthquake ( $M_w$  7.7 by USGS and  $M_w$  7.6 by JMA), the 2011 Miyagi-oki earthquake of a possible foreshock for the 2011 Tohoku earthquake ( $M_w$  7.3, written as Tohoku-f in the figure), and the 2011 Tohoku earthquake ( $M_w$  9.0). The contours represent the depths of the plate interface (Hayes *et al.* 2012) at 40 km intervals.

foreshock for the 2011 Tohoku earthquake ( $M_w$  7.3, written as Tohoku-f in the figure), and the 2011 Tohoku earthquake ( $M_w$  9.0).

We extract the slip velocity of early phases of the afterslip from previous studies. Miyazaki & Larson (2008) calculated fault slip during 70 min just after the main shock of the 2003 Tokachi-oki earthquake. The slip amount was 2–4 cm, thus the mean slip velocity was about  $5 \times 10^{-6}$ – $1 \times 10^{-5}$   $\text{m s}^{-1}$ . Ohta *et al.* (2012) constructed an afterslip model for the 2011 Miyagi-oki earthquake. The slip amount for 51 hr (the time span between this foreshock and the main shock of the 2011 Tohoku earthquake) was 20–40 cm. Although the time span in this case was far longer than the other cases, we assessed the length effect (time decay of the afterslip) was at most two or three times, from their original time-series data. The corresponding mean slip velocity was  $1 \times 10^{-6}$ – $2 \times 10^{-6}$   $\text{m s}^{-1}$ . In addition, we roughly estimate amount of early afterslip of the 1994 Sanriku-oki earthquake from the strainmeter data used in Heki & Tamura (1997) (Appendix B). The mean slip velocity was  $4 \times 10^{-6}$ – $7 \times 10^{-6}$   $\text{m s}^{-1}$  (true values may be slightly larger because we did not use the oscillating time-series data immediately after the main shock). Note that acceleration of the Pacific Plate subduction after the 2003 Tokachi-oki earthquake and the 2011 Tohoku-oki earthquake (Heki & Mitsui 2013) did not affect the slip velocity of the afterslip, because the increased amounts of the plate subduction rate were the same order of magnitude as the ordinary subduction rate ( $\sim 10^{-9}$   $\text{m s}^{-1}$ ).

Fig. 10 shows the compiled result for the mean slip velocity of the early afterslip versus the moment magnitude of main shock. We find that the case of the 2011 Tohoku earthquake has one order of magnitude higher slip velocity than the others. Also we find an increasing trend of the afterslip velocity for the main shock magnitude. For example, a scaling relation of  $v_{af} \propto 10^{M_w}$  or  $v_{af} \propto M_o^{2/3}$ , where  $v_{af}$  is the slip velocity of early afterslip and  $M_o$  is the seismic moment, could be realized. The dependence is similar to the scaling relation of aftershock numbers for the main shock magni-



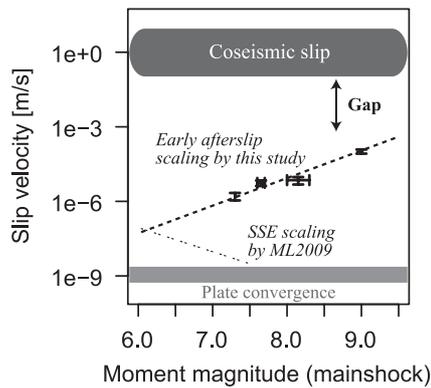
**Figure 10.** A compiled result for the mean slip velocity of early afterslip versus the moment magnitude of main shock at the Pacific subduction plate interface (the 2011 Tohoku earthquake of  $M_w$  9.0; the 2003 Tokachi-oki earthquake of  $M_w$  8.0–8.3; the 1994 Sanriku-oki earthquake of  $M_w$  7.6–7.7, the 2011 Miyagi-oki earthquake of  $M_w$  7.3. Note that only the result of the 2011 Miyagi-oki earthquake was based on the longer-period (almost 2 d) data than the others.

tude of interplate earthquakes in Japan (Yamanaka & Shimazaki 1990). This fact may indicate correlations of afterslip and aftershocks, for example as proposed by Matsuzawa (2004), though all of those phenomena are not necessarily occur on interplate faults.

We also note that the increasing trend of the early afterslip velocity for the main shock magnitude is different from the decreasing trend of SSE (spontaneous slow slip event) velocity for its magnitude by Meade & Loveless (2009). According to the discussion of Meade & Loveless (2009), the decreasing trend of the SSE velocity is explained by the following facts: (1) Larger SSEs have larger source areas. (2) Linear relation of seismic moment and event duration (namely, constant moment release rate) of SSE (Ide *et al.* 2007). In contrast, we confirmed non-constant moment release rate of the early afterslip by checking slip area in the above-mentioned cases as well as the slip velocity. The moment release rate of the early afterslip also increases with the increasing main shock magnitude. The increasing trend of the early afterslip is not strange, because stressing rates at edges of larger main shock faults should be higher.

The value  $10^{-4}$   $\text{m s}^{-1}$  in the case of the 2011 Tohoku earthquake ( $M_9.0$ ) implies an effective maximal velocity for afterslip phenomena. In contrast, the coseismic slip velocity of earthquakes is as fast as  $10^{-1}$  to  $10^1$   $\text{m s}^{-1}$  (e.g. Heaton 1990; Yomogida & Nakata 1994; Yagi & Fukahata 2011). There is a gap of over 3 orders of magnitude of the slip velocity between afterslip and coseismic slip. Fig. 11 illustrates the above points.

The gap between the afterslip and seismic values may reflect properties of friction on faults. Based on rock experiments using Granite, Weeks (1993) proposed that steady-state friction turns into velocity-strengthening behaviour around  $10^{-4}$   $\text{m s}^{-1}$  from velocity-weakening behaviour in the lower-velocity range. This point seems consistent with our implication for the maximal afterslip velocity  $10^{-4}$   $\text{m s}^{-1}$ . The gap might be explained by drastic frictional weakening at very high speeds (e.g. Sibson 1973; Tsutsumi & Shimamoto 1997; Di Toro *et al.* 2011), associated with complex frictional processes, for instance, ‘competition’ among the change in velocity dependence of steady-state friction, porosity evolution within fault gouge, thermal fluid pressurization due to shear heating, and diffusion of heat and fluid (Mitsui & Cocco 2010).



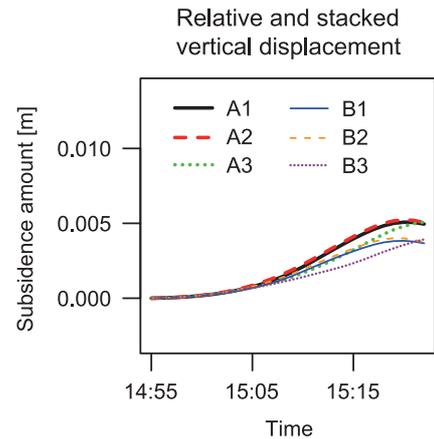
**Figure 11.** A schematic of the relations among velocity of the afterslip at the Pacific subduction plate interface (the same data as Fig. 10), seismic slip, and plate convergence. The gap exists between the afterslip and seismic slip over 3 orders of the slip velocity. The plotted line for the early afterslip scaling is  $v_{af} \propto 10^{M_w}$  ( $v_{af} \propto M_0^{2/3}$ ), where  $v_{af}$  is the early afterslip velocity and  $M_0$  is the seismic moment. In order to compare with the early afterslip, we also plot another scaling relation for SSE (spontaneous slow slip event) proposed by Meade & Loveless (2009) (named as ML2009 in the figure). The early afterslip is the increasing trend for the main shock magnitude, but the SSE is the decreasing trend for its magnitude.

### 3.2 Examination of vertical deformation amount due to tsunami load

In the previous Section 2.3, we simulated that only the coastal stations subsided by subcentimetre due to sea-mass loads based on the tsunami simulation (Gusman *et al.* 2012). The subsidence amounts of stations 0171 and 0550 reached almost 1 cm. The amounts are not negligible but still not sufficiently large values to be detected by GPS robustly. Here we further examine the amounts of the tsunami-induced subsidence.

First, we investigate effects of the assumed velocity structure to calculate the surface-load deformation. All of the above calculations were based on the PREM (Dziewonski & Anderson 1981). As an alternative velocity structure model, we try two earth structure models: the Gutenberg–Bullen A model (Alterman *et al.* 1961) and the 1066A model [Gilbert & Dziewonski (1975), where the Green’s function was given by Okubo & Saito (1983) and Endo & Okubo (1984)]. We call three models as A1, A2 and A3, respectively. Moreover, we test another tsunami simulation model (Satake *et al.* 2013) as a source of the surface loads. We also name three models with the different earth structure models as B1, B2 and B3. In order to compare the six models, we calculate relative subsidence amounts of the coastal stations (0906, 0028, 0167, 0170, 0171, 0172 and 0550) from the landward stations (0547, 0169, 0546, 0911, 0914, 0918 and 0549). We stack the simulated values for the coastal stations and the landward stations, respectively, to take their difference. Fig. 12 shows the temporal evolution in the relative subsidence for each model. We find that the model uncertainties do not alter the calculation results so much.

Second, we speculate that permanent seafloor deformation owing the main shock (Tsushima *et al.* 2012) caused non-negligible subsidence, via permanent sea-mass movement above the deformed seafloor. Here we call this deformation as ‘secondary’ vertical displacement, where ‘primary’ vertical displacement is directly caused by the main shock fault slip. Our previous calculations were based on the tsunami simulations of which initial conditions were sea-



**Figure 12.** The simulated temporal evolution of the relative subsidence for each model: A1 (based on the Gusman *et al.* (2012) simulation with the PREM), A2 (with Gutenberg–Bullen A model), A3 (with the 1066A model), B1 (based on the Satake *et al.* (2013) simulation with the PREM), B2 (with Gutenberg–Bullen A model) and B3 (with the 1066A model). We calculate the relative subsidence by subtracting the stacked subsidence amount at the landward stations from that at the coastal stations.

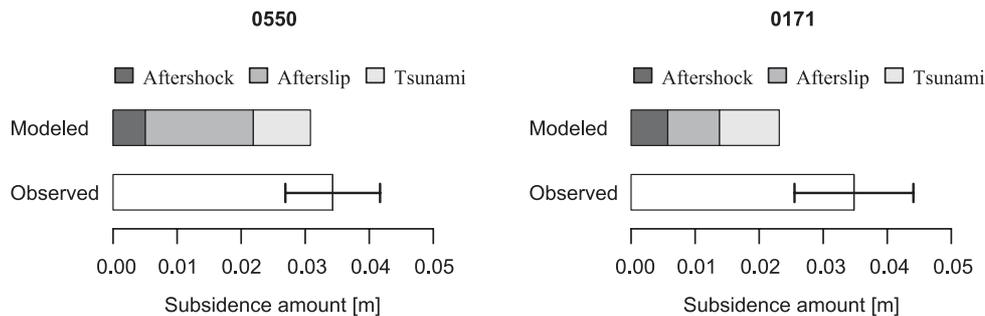
height changes due to the primary displacement, thus they did not consider the permanent sea-mass movement and the secondary displacement. In order to estimate the amount of the secondary vertical displacement, we check the primary vertical displacement in the 2011 Tohoku earthquake. For example, Simons *et al.* (2011) revealed that the primary vertical displacement near the Sanriku coast was as large as several metres subsidence. This coseismic subsidence led to permanent sea-mass increases above the region. By a rough calculation using the boundary element method (Farrell 1972) with the Green’s function (Pagiatakis 1990), we find that the subsidence amount of the secondary vertical displacement along the Sanriku coast reached several millimetres, a little less than the previously simulated subsidence amount. This fact implies: (1) the total amount of the tsunami-induced subsidence could be twice the amount of the calculated values from the tsunami simulation, since the permanent sea-mass movement do not occur immediately after the main shock. (2) the tsunami-induced subsidence does not necessarily vanish after the finish of the tsunami phenomenon (transient wave).

Of course, for more quantitative discussion, we should consider other factors such as dynamic loading effects (e.g. Okubo & Tsuji 2001), meridian changes at the observation points, or size effects of the simulation grids near the coast. Moreover, water inundation and run-up inland to several kilometres (Mori *et al.* 2011), which were not implemented in the referred simulation, would increase the subsidence amounts at the GPS stations.

### 3.3 Possibility of detection of tsunami-induced subsidence

As was discussed above, we expected that the vertical displacement due to the tsunami-loading was at most 1 cm or more, at coastal stations 0550 and 0171. We consider the possibility of the detection of the tsunami-induced subsidence at these two stations.

Fig. 13 shows comparative results between the observed subsidence (Fig. 2) and modelled subsidence due to the aftershocks, afterslip and tsunami at stations 0550 and 0171. The model of the



**Figure 13.** Comparative results between the observed subsidence with the error bars (Fig. 2) and modelled subsidence due to the aftershocks, afterslip and tsunami at coastal stations 0550 and 0171. The model of the afterslip deformation is the least  $S_1$  model, and the tsunami deformation is model A1.

afterslip deformation is the least  $S_1$  model, and the tsunami deformation is model A1.

We find that the tsunami-induced subsidence might reach tens of percent of the observed subsidence amounts at the two coastal stations. The predicted subsidence amounts account for a large portion of the residuals between the observation and the modelled deformation due to the fault slip. On the other hand, model uncertainties of the fault slip phenomena (aftershocks and afterslip) could exceed the tsunami-induced signals. It means that further discussion is difficult without detailed models of the fault slip phenomena in this condition.

#### 4 CONCLUSION

We checked the on-land GPS data along the Sanriku coast during almost 30 min after the  $M_w$  9 Tohoku earthquake, where the tsunami had the largest amplitude. The  $M_w$  7-class aftershocks, the afterslip and the tsunami caused land deformation, respectively. First, we modelled the early phase of the afterslip. The mean slip velocity of the early afterslip reached  $0.1 \text{ mm s}^{-1}$ . This value is one-order larger than the early afterslip of the recent large earthquakes at the Pacific subduction plate interface. We found that the early afterslip velocity  $v_{af}$  had the increasing trend with the main shock magnitude. This analysis implied  $v_{af} \propto M_o^{2/3}$  ( $M_o$  is the seismic moment of the main shock). Next, we calculated the tsunami-induced deformation based on the tsunami simulation models. The expected subsidence amounts at some coastal stations were as large as 1 cm, which can explain a large part of the gaps between the observation and the modelled slip-induced deformation.

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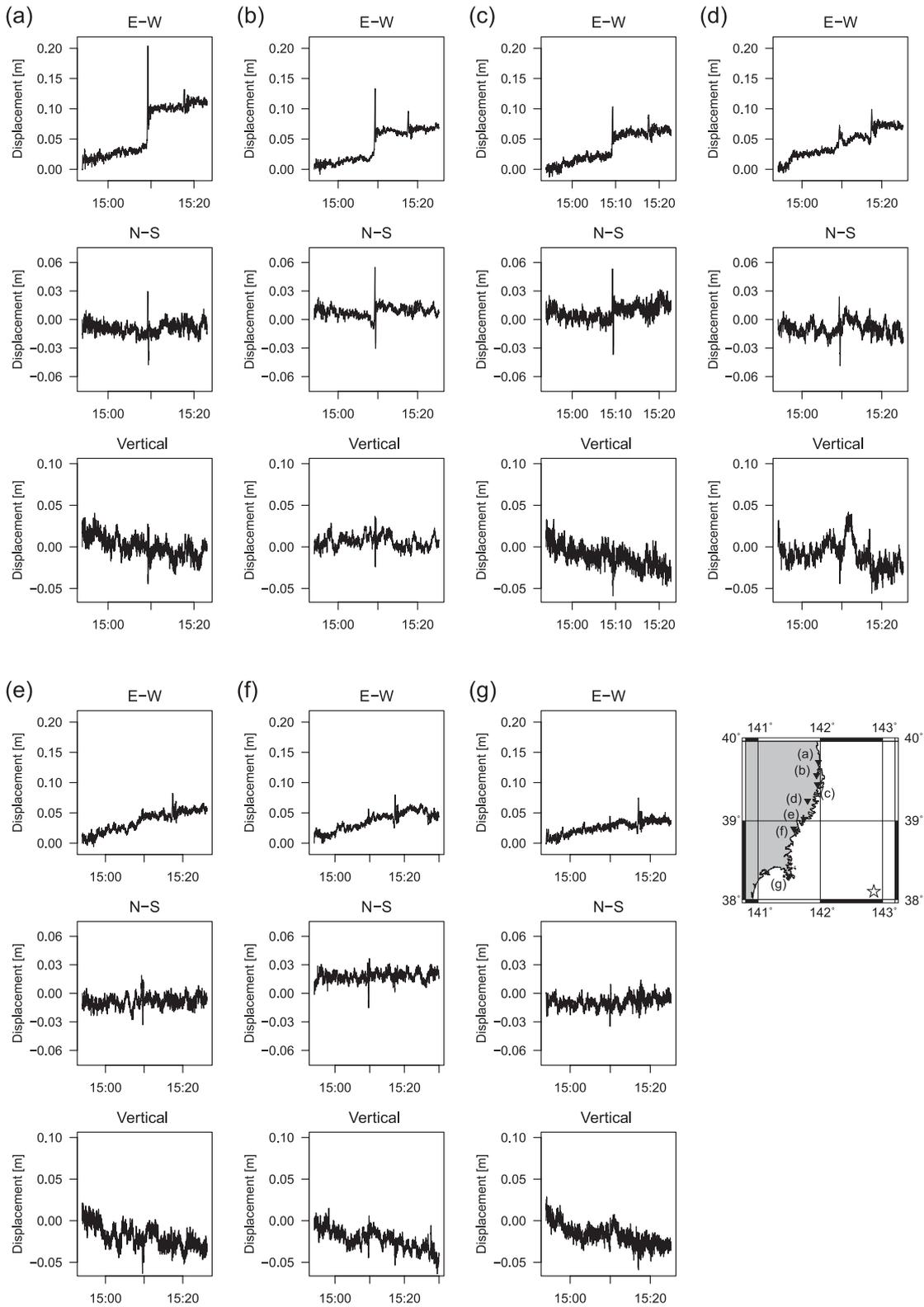
## APPENDIX A: GPS TIME-SERIES DATA AFTER THE 2011 TOHOKU EARTHQUAKE

Figs A1 and A2 show the relative displacement at the coastal and landward GEONET stations from 14:54, on 2011 March 11, in the east–west (E–W), north–south (N–S), and vertical directions.

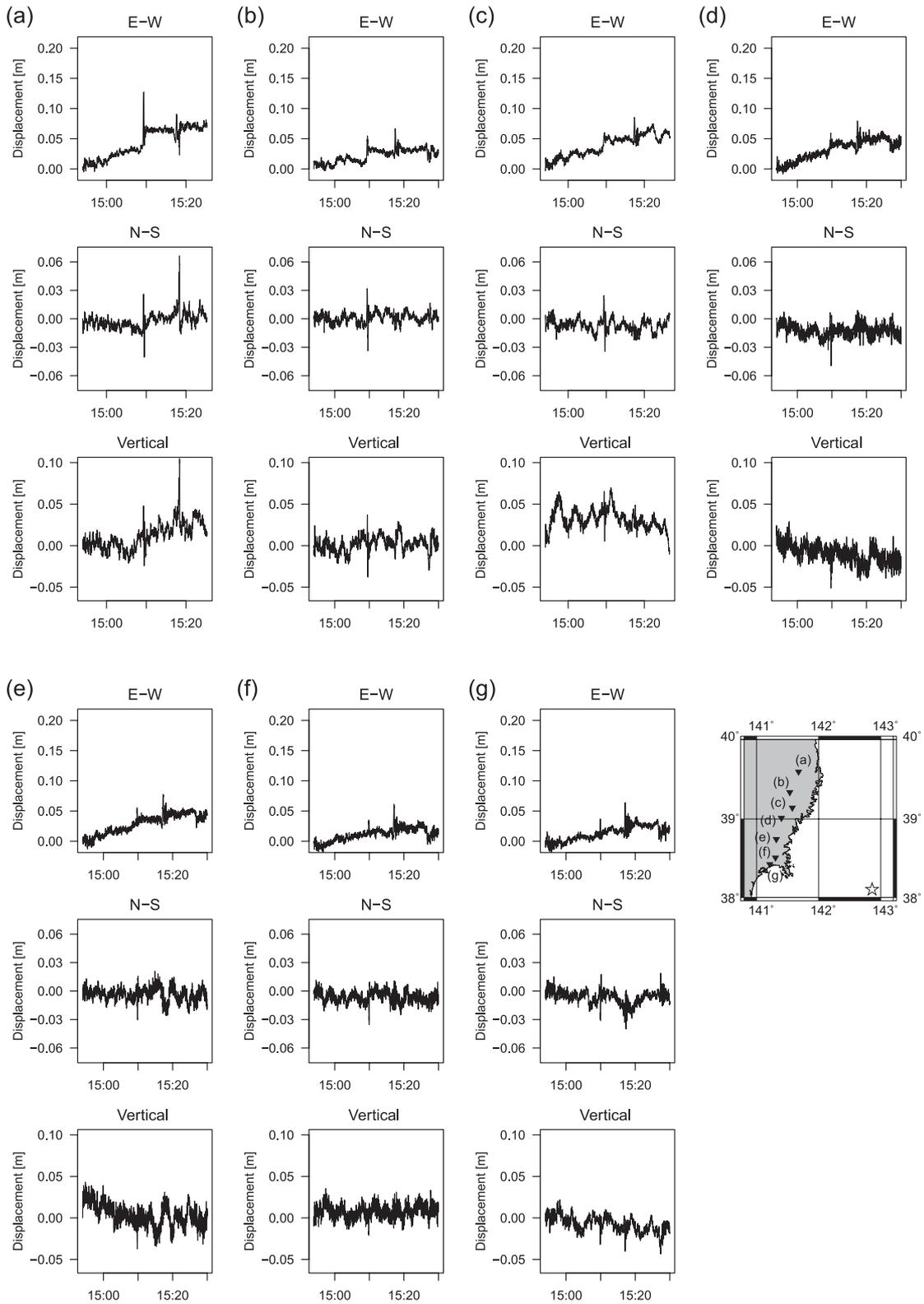
## APPENDIX B: EARLY AFTERSLIP OF THE 1994 SANRIKU-OKI EARTHQUAKE

We estimate the slip amount of early afterslip in the case of the 1994 Sanriku-oki earthquake. We use an extensometer at the Esashi Earth Tide Station (EETS, 141.34°E, 39.15°N) near the source area. The extensometer provided strain data every 10 min with less noise than GPS at that time, which is useful to investigate the early afterslip (Heki & Tamura 1997). Fig. B1 shows the location of the station and the afterslip fault model by Heki *et al.* (1997).

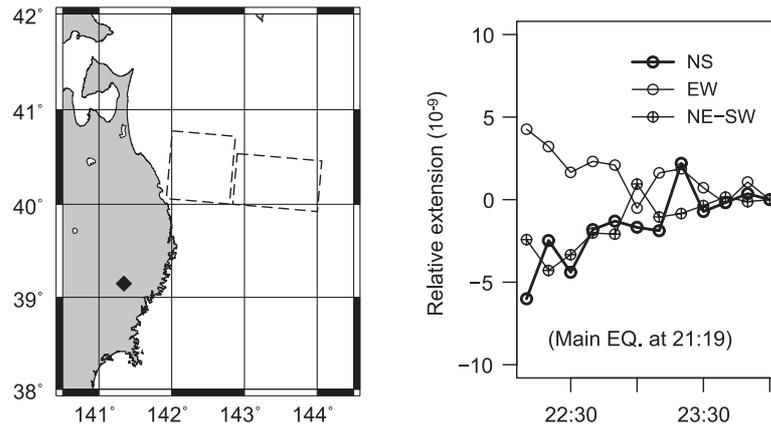
We focus on the early phase of the afterslip during 2 hr starting almost 1 hr after the main shock (because the time-series data immediately after the main shock oscillated). Fig. B1 also presents the time-series data in three horizontal components (north–south, east–west, and northern east–southern west). Using the Green's function in a homogeneous elastic half-space (Okada 1992) and the afterslip model by Heki *et al.* (1997), we find that dislocation of 3–5 cm at the model faults explain the data. The corresponding mean slip velocity is  $4 \times 10^{-6}$  to  $7 \times 10^{-6}$  m s $^{-1}$ .



**Figure A1.** Three-direction relative displacement at the coastal stations: (a) at 0906 station; (b) at 0028 station; (c) at 0167 station; (d) at 0170 station; (e) at 0171 station; (f) at 0172 station and (g) at 0550 station. Most of the time-series data did not continue up to 15:30, owing to electric outages by tsunami arrivals. Only the data at 0172 station remained. The lowest right-hand panel illustrates the station locations.



**Figure A2.** Three-direction relative displacement at the landward stations: (a) at 0547 station; (b) at 0169 station; (c) at 0546 station; (d) at 0911 station; (e) at 0914 station; (f) at 0918 station and (g) at 0549 station. The time-series data at 0546 and 0547 stations were not continuous up to 15:30. The lowest right-hand panel illustrates the station locations.



**Figure B1.** Left-hand panel: the location of the extensometer at EETS station represented by the solid rhombus, and the fault model of the afterslip by Heki *et al.* (1997). Right-hand panel: the extensometer data during 2 hr from almost 1 hr after the main shock. The relative extension in each component means the relative values from those at 24:00. The time zone is JST.